



Structural Calculations

for

Site: Fred JMG Realty
1900 Southeast Hillmoor Drive
Port St. Lucie, FL 329966

Project: 20.0' x 24.0'
Shed
Inv. No. 1665567

Store: 520 - Orlando
8524 East Colonial Drive
Orlando, FL 32817

Engineer: Timothy Cahalan, P.E.
Tuff Shed Inc.
1777 South Harrison St., Ste. 600
Denver, CO 80210
(303) 753-8833 ext. 96319
TCahalan@tuffshed.com

Date: July 21, 2021



DESIGN CRITERIA

Building Code: 2020 FBC (7th Ed.)
Seismic Design Category: A
Basic Wind Speed: 160 mph
Wind Exposure: C

Building Specifications

Width: 20.0 ft.
Length: 24.0 ft.
Side Wall Height: 8.09 ft.
Stud Size: 2x4
Stud Spacing: 16 in. o.c.
Wall Sheathing: 3/8" Smartside
Roof Sheathing: 7/16" OSB
Wall Wood Species & Grade: SPF #1/#2
Wall "A" Overhang: .0 in.
Wall "B" Overhang: 12.0 in.
Wall "C" Overhang: .0 in.
Wall "D" Overhang: 12.0 in.
Foundation: Treated Wood Shed Base
Anchor:
Anchor Bolt Diameter: .0 in.

Trusses

Span: 20.0 ft.
Left Overhang: 12.0 in.
Right Overhang: 12.0 in.

Pitch: 4./12
Lumber: SPF #1/#2
Roofing: Composition Shingles
Top Chord Live/Snow Load: 20 psf
Top Chord Dead Load: 10 psf
Bottom Chord Live Load: 0 psf
Bottom Chord Dead Load: 10 psf

Risk Category: I - Low Hazard

Header: Wall A, Hdr 1

Top Chord Live/Snow Load: 20 psf Top Chord Dead Load: 10 psf Bottom Chord Live Load: 0 psf Bottom Chord Dead Load: 10 psf		Tributary Width= 1.50 ft. Height of wall above Header= 3.0 ft. Moment= 9,754 in.-lbs. Reaction= 383 lbs.	
Header Size: 2x6 Number of Headers: 2 Header depth= 5.50 in. Total header width= 3.0 in. Header span= 8.50 ft.		Header Size: 1½x3½ LVL Number of Headers: 2 Header depth= 3.50 in. Total header width= 3.50 in. Header span= 8.50 ft.	
Lumber SPF #1/#2		Lumber LVL 2600Fb	
F _b = 875 psi F _t = 450 psi F _v = 135 psi F _{cp} = 425 psi F _c = 1150 psi E= 1,400,000 psi E _{min} = 510,000 psi		F _b = 2600 psi F _t = 1555 psi F _v = 285 psi F _{cp} = 750 psi F _c = 2510 psi E= 1,900,000 psi E _{min} = 965,710 psi	
<i>Bending</i> S _x = 15.13 cu.in. F' _b = 1398 psi f _b = 645 psi		<i>Bending</i> S _x = 7.15 cu.in. F' _b = 3224 psi f _b = 1365 psi	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
<i>Shear</i> F' _v = 169 psi f _v = 35 psi		<i>Shear</i> F' _v = 356 psi f _v = 47 psi	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
<i>Deflection</i> E'= 1,400,000 psi I= 41.594 Deflection Ratio= L/180 Allowable Deflection= .57 in. Δ= .18 in.		<i>Deflection</i> E'= 1,900,000 psi I= 12.505 Deflection Ratio= L/180 Allowable Deflection= .57 in. Δ= .44 in.	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
Lumber Factors C _D = 1.25 Duration C _M = 1.00 Wet Service C _t = 1.00 Temperature C _i = 0.98 Beam Stability C _F = 1.30 Size C _{fu} = 1.00 Flat Use C _i = 1.00 Incising C _r = 1.00 Repetitive Member C _r = 1.00 Form TL (L/x) L/240 LL(L/x) .43 in. .12 in.		Lumber Factors C _D = 1.25 Duration C _M = 1.00 Wet Service C _t = 1.00 Temperature C _i = 0.99 Beam Stability C _F = 1.00 Size C _{fu} = 1.00 Flat Use C _i = 1.00 Incising C _r = 1.00 Repetitive Member C _r = 1.00 Form TL(L/x) L/240 LL(L/x) .57 in. .30 in.	

Header: Wall B, Hdr 1

Top Chord Live/Snow Load: 20 psf Top Chord Dead Load: 10 psf Bottom Chord Live Load: 0 psf Bottom Chord Dead Load: 10 psf		Tributary Width= 11.0 ft. Height of wall above Header= 1.50 ft. Moment= 7,209 in.-lbs. Reaction= 739 lbs.	
Header Size: 2x4 Number of Headers: 2 Header depth= 3.50 in. Total header width= 3.0 in. Header span= 3.25 ft.		Header Size: 1½x3½ LVL Number of Headers: 2 Header depth= 3.50 in. Total header width= 3.50 in. Header span= 3.25 ft.	
Lumber SPF #1/#2		Lumber LVL 2600Fb	
F _b = 875 psi F _t = 450 psi F _v = 135 psi F _{cp} = 425 psi F _c = 1150 psi E= 1,400,000 psi E _{min} = 510,000 psi		F _b = 2600 psi F _t = 1555 psi F _v = 285 psi F _{cp} = 750 psi F _c = 2510 psi E= 1,900,000 psi E _{min} = 965,710 psi	
<i>Bending</i> S _x = 6.13 cu.in. F' _b = 1634 psi f _b = 1177 psi		<i>Bending</i> S _x = 7.15 cu.in. F' _b = 3240 psi f _b = 1009 psi	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
<i>Shear</i> F' _v = 169 psi f _v = 106 psi		<i>Shear</i> F' _v = 356 psi f _v = 91 psi	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
<i>Deflection</i> E'= 1,400,000 psi I= 10.71875 Deflection Ratio= L/180 Allowable Deflection= .22 in. Δ= .08 in.		<i>Deflection</i> E'= 1,900,000 psi I= 12.50520833 Deflection Ratio= L/180 Allowable Deflection= .22 in. Δ= .05 in.	
<i>Good/No Good?</i> O.K.		<i>Good/No Good?</i> O.K.	
Lumber Factors C _D = 1.25 Duration C _M = 1.00 Wet Service C _t = 1.00 Temperature C _i = 1.00 Beam Stability C _F = 1.50 Size C _{fu} = 1.00 Flat Use C _i = 1.00 Incising C _r = 1.00 Repetitive Member C _r = 1.00 Form TL (L/x) L/240 LL(L/x) .16 in. .04 in.		Lumber Factors C _D = 1.25 Duration C _M = 1.00 Wet Service C _t = 1.00 Temperature C _i = 1.00 Beam Stability C _F = 1.00 Size C _{fu} = 1.00 Flat Use C _i = 1.00 Incising C _r = 1.00 Repetitive Member C _r = 1.00 Form TL(L/x) L/240 LL(L/x) .22 in. .02 in.	

Header: Wall B, Hdr 2

Top Chord Live/Snow Load: 20 psf Top Chord Dead Load: 10 psf Bottom Chord Live Load: 0 psf Bottom Chord Dead Load: 10 psf			Tributary Width= 11.0 ft. Height of wall above Header= 1.50 ft. Moment= 12,328 in.-lbs. Reaction= 967 lbs.		
Header Size: 2x6 Number of Headers: 2 Header depth= 5.50 in. Total header width= 3.0 in. Header span= 4.25 ft.			Header Size: 1½x3½ LVL Number of Headers: 2 Header depth= 3.50 in. Total header width= 3.50 in. Header span= 4.25 ft.		
Lumber SPF #1/#2			Lumber LVL 2600Fb		
<i>Bending</i> $S_x = 15.13 \text{ cu.in.}$ $F'_b = 1410 \text{ psi}$ $f_b = 815 \text{ psi}$			<i>Bending</i> $S_x = 7.15 \text{ cu.in.}$ $F'_{cp} = 3237 \text{ psi}$ $f_b = 1725 \text{ psi}$		
$F_b = 875 \text{ psi}$ $F_t = 450 \text{ psi}$ $F_v = 135 \text{ psi}$ $F_{cp} = 425 \text{ psi}$ $F_c = 1150 \text{ psi}$ $E = 1,400,000 \text{ psi}$ $E_{min} = 510,000 \text{ psi}$			$F_b = 2600 \text{ psi}$ $F_t = 1555 \text{ psi}$ $F_v = 285 \text{ psi}$ $F_{cp} = 750 \text{ psi}$ $F_c = 2510 \text{ psi}$ $E = 1,900,000 \text{ psi}$ $E_{min} = 965,710 \text{ psi}$		
<i>Good/No Good?</i> O.K.			<i>Good/No Good?</i> O.K.		
<i>Shear</i> $F'_v = 169 \text{ psi}$ $f_v = 88 \text{ psi}$			<i>Shear</i> $F'_v = 356 \text{ psi}$ $f_v = 118 \text{ psi}$		
$C_D = 1.25$ $C_M = 1.00$ $C_t = 1.00$ $C_L = 0.99$ $C_F = 1.30$ $C_{fu} = 1.00$ $C_i = 1.00$ $C_r = 1.00$ $C_t = 1.00$			$C_D = 1.25$ $C_M = 1.00$ $C_t = 1.00$ $C_L = 1.00$ $C_F = 1.00$ $C_{fu} = 1.00$ $C_i = 1.00$ $C_r = 1.00$ $C_t = 1.00$		
<i>Deflection</i> $E' = 1,400,000 \text{ psi}$ $I = 41.59375$ Deflection Ratio= L/180 Allowable Deflection= .28 in. $\Delta = .06 \text{ in.}$			<i>Deflection</i> $E' = 1,900,000 \text{ psi}$ $I = 12.50520833$ Deflection Ratio= L/180 Allowable Deflection= .28 in. $\Delta = .14 \text{ in.}$		
<i>Good/No Good?</i> O.K.			<i>Good/No Good?</i> O.K.		
Lumber Factors Duration Wet Service Temperature Beam Stability Size Flat Use Incising Repetitive Member Form LL(L/x)			Lumber Factors Duration Wet Service Temperature Beam Stability Size Flat Use Incising Repetitive Member Form LL(L/x)		
O.K.			O.K.		

OR

<p>Trimmer for: Header: Wall A, Hdr 1</p> <p>SPF #1/#2</p> <p>$F_b = 875$ psi $F_t = 450$ psi $F_v = 135$ psi $F_{cp} = 425$ psi $F_c = 1150$ psi $E_{min} = 510,000$ psi</p> <p>Load= 383 lbs. width= 3.50 in. thickness= 1.50 in. No. of members= 1 Unbraced Length(x)(width)= 89.13 in. Unbraced Length(y)(thickness)= 6.0 in. Effective Length factor, $K_{e(x)} = 1$ Effective Length factor, $K_{e(y)} = 1$</p> <p>$c = 0.8$ $A = 5.25$ sq.in. $(l/d)_x = 25.46$ $(l/d)_y = 4.00$ $E'_{min} = 510,000$ psi</p> <p>Lumber Factors</p> <p>$C_D = 1.25$ Duration $C_M = 1.00$ Wet Service $C_t = 1.00$ Temperature $C_L = 1.00$ Beam Stability $C_F = 1.15$ Size $C_{fu} = 1.00$ Flat Use $C_i = 1.00$ Incising $C_r = 1.00$ Repetitive Member $C_f = 1.00$ Form $C_T = 1.00$ Buckling Stiffness</p> <p>Weak Axis Calculations(y)</p> <p>$F_{ce} = 26201.25$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 15.85$ $1+F_{ce}/F^*_c/2c = 10.53$ $C_P = 0.99$ $F'_c = 1631.46$ $P_{allowable} = 8,565$ lbs.</p> <p>Strong Axis Calculations (x)</p> <p>$F_{ce} = 646.52$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 0.39$ $1+F_{ce}/F^*_c/2c = 0.87$ $C_P = 0.35$ $F'_c = 582.99$ $P_{allowable} = 3,061$ lbs.</p> <p>Good/No Good? O.K.</p>	<p>Trimmer for: Header: Wall B, Hdr 1</p> <p>SPF #1/#2</p> <p>$F_b = 875$ psi $F_t = 450$ psi $F_v = 135$ psi $F_{cp} = 425$ psi $F_c = 1150$ psi $E_{min} = 510,000$ psi</p> <p>Load= 739 lbs. width= 3.50 in. thickness= 1.50 in. No. of members= 1 Unbraced Length(x)(width)= 89.13 in. Unbraced Length(y)(thickness)= 6.0 in. Effective Length factor, $K_{e(x)} = 1$ Effective Length factor, $K_{e(y)} = 1$</p> <p>$c = 0.8$ $A = 5.25$ sq.in. $(l/d)_x = 25.46$ $(l/d)_y = 4.00$ $E'_{min} = 510,000$ psi</p> <p>Lumber Factors</p> <p>$C_D = 1.25$ Duration $C_M = 1.00$ Wet Service $C_t = 1.00$ Temperature $C_L = 1.00$ Beam Stability $C_F = 1.15$ Size $C_{fu} = 1.00$ Flat Use $C_i = 1.00$ Incising $C_r = 1.00$ Repetitive Member $C_f = 1.00$ Form $C_T = 1.00$ Buckling Stiffness</p> <p>Weak Axis Calculations(y)</p> <p>$F_{ce} = 26201.25$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 15.85$ $1+F_{ce}/F^*_c/2c = 10.53$ $C_P = 0.99$ $F'_c = 1631.46$ $P_{allowable} = 8,565$ lbs.</p> <p>Strong Axis Calculations (x)</p> <p>$F_{ce} = 646.52$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 0.39$ $1+F_{ce}/F^*_c/2c = 0.87$ $C_P = 0.35$ $F'_c = 582.99$ $P_{allowable} = 3,061$ lbs.</p> <p>Good/No Good? O.K.</p>
<p>Trimmer for: Header: Wall B, Hdr 2</p> <p>SPF #1/#2</p> <p>$F_b = 875$ psi $F_t = 450$ psi $F_v = 135$ psi $F_{cp} = 425$ psi $F_c = 1150$ psi $E_{min} = 510,000$ psi</p> <p>Load= 967 lbs. width= 3.50 in. thickness= 1.50 in. No. of members= 1 Unbraced Length(x)(width)= 89.13 in. Unbraced Length(y)(thickness)= 6.0 in. Effective Length factor, $K_{e(x)} = 1$ Effective Length factor, $K_{e(y)} = 1$</p> <p>$c = 0.8$ $A = 5.25$ sq.in. $(l/d)_x = 25.46$ $(l/d)_y = 4.00$ $E'_{min} = 510,000$ psi</p> <p>Lumber Factors</p> <p>$C_D = 1.25$ Duration $C_M = 1.00$ Wet Service $C_t = 1.00$ Temperature $C_L = 1.00$ Beam Stability $C_F = 1.15$ Size $C_{fu} = 1.00$ Flat Use $C_i = 1.00$ Incising $C_r = 1.00$ Repetitive Member $C_f = 1.00$ Form $C_T = 1.00$ Buckling Stiffness</p> <p>Weak Axis Calculations(y)</p> <p>$F_{ce} = 26201.25$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 15.85$ $1+F_{ce}/F^*_c/2c = 10.53$ $C_P = 0.99$ $F'_c = 1631.46$ $P_{allowable} = 8,565$ lbs.</p> <p>Strong Axis Calculations (x)</p> <p>$F_{ce} = 646.52$ $F^*_c = 1653.13$ $F_{ce}/F^*_c = 0.39$ $1+F_{ce}/F^*_c/2c = 0.87$ $C_P = 0.35$ $F'_c = 582.99$ $P_{allowable} = 3,061$ lbs.</p> <p>Good/No Good? O.K.</p>	

Wind Calculations (C&C)

Alternate all-heights method

Wind Speed, v_{ASD} : 124 mph

Wind Exposure: C

Risk Category: I - Low Hazard

Roof Angle= 18.43

Gable Wall Span= 20.0 ft.

Longitude Wall Span= 24.0 ft.

Enclosure Classification: Enclosed

Section 26.10

K_{zt} = 1

Section 26.8.2

K_t = 0.85

Table 27.3-1

K_d = 0.85

Table 26.6-1

Mean Roof Height= 11.42 ft.

LOW RISE BUILDINGS (ASCE 7-16 Chapt. 30)

GC_{pi} = 0.18

q_h = 28.41 psf

	<u>Zone 1</u>	<u>Zone 2</u>	<u>Zone 3</u>	<u>Zone 4</u>	<u>Zone 5</u>	
GC_p =	-0.9	-1.7	-2.6	-1.1	-1.4	(ASCE 7-16 Figures 30.3-1,30.3-2B,30.3-2a,30.3-2C)
GC_p =	0.5	0.5	0.5	1.0	1.0	(ASCE 7-16 Figures 30.3-1,30.3-2B,30.3-2a,30.3-2C)

p =	-30.68 psf	-53.41 psf	-78.98 psf	-36.36 psf	-44.89 psf
p =	19.32 psf	19.32 psf	19.32 psf	33.52 psf	33.52 psf
p =	-30.68 psf	-53.41 psf	-78.98 psf	-36.36 psf	-44.89 psf
p =	19.32 psf	19.32 psf	19.32 psf	33.52 psf	33.52 psf
p_{max} =	19 psf	19 psf	19 psf	34 psf	34 psf
p_{min} =	-31 psf	-53 psf	-79 psf	-36 psf	-45 psf

Wind Calculations (MWFRS)

ASCE 7-16 Chapt. 28 Part 1

Wind Speed, v_{ASD} : 124 mph
 Wind Speed, v_{ULT} : 160 mph
 Wind Exposure: C
 Risk Category: I - Low Hazard
 Roof Angle= 18.43
 Gable Wall Span= 20.0 ft.
 Longitude Wall Span= 24.0 ft.
 Mean Roof Height= 11.42 ft.
 Enclosure Classification: Enclosed
 K_{zt} = 1
 K_r = 0.85
 K_d = 0.85

Section 26.10
 Section 26.8.2
 Table 27.3-1
 Table 26.6-1

GC_{pi} = ±0.18
 q_n = 47.35 psf

Table 26.11-1
 Eq. 28.3-1

C_e		1	2	3	4	5	6	1E	2E	3E	4E	5E	6E
0	Load Case A	0.52	-0.69	-0.47	-0.42	N/A	N/A	0.78	-1.07	-0.67	-0.62	N/A	N/A
	Load Case B	-0.45	-0.69	-0.37	-0.45	0.40	-0.29	-0.48	-1.07	-0.53	-0.48	0.61	-0.43
D	Load Case A (- GC_{pi})	15.93 psf	-41.19 psf	-30.71 psf	-28.19 psf	N/A	N/A	28.42 psf	-59.19 psf	-40.40 psf	-37.79 psf	N/A	N/A
	Load Case A (+ GC_{pi})	32.97 psf	-24.15 psf	-13.66 psf	-11.14 psf	N/A	N/A	45.46 psf	-42.14 psf	-23.36 psf	-20.74 psf	N/A	N/A
	Load Case B (- GC_{pi})	-29.83 psf	-41.19 psf	-26.04 psf	-29.83 psf	10.42 psf	-22.25 psf	-31.25 psf	-59.19 psf	-33.62 psf	-31.25 psf	20.36 psf	-28.88 psf
	Load Case B (+ GC_{pi})	-12.78 psf	-24.15 psf	-9.0 psf	-12.78 psf	27.46 psf	-5.21 psf	-14.20 psf	-42.14 psf	-16.57 psf	-14.20 psf	37.41 psf	-11.84 psf

max. p_s = 45.46 psf Side Wall, maximum wind pressure
 max. p_t = 37.41 psf Gable End Wall, maximum wind pressure

max. p_{roof} = -59.19 psf

V_L = 4,273 lbs. Max. Longitudinal Shear
 V_T = 6,232 lbs. Max. Transversal Shear

Max. uplift pressure= -31,251 lbs. Max. uplift pressure on the building due to wind on roof

Diaphragm Calculations

Length (for shear)

Wall A: 12.0 ft.
 Wall B: 17.0 ft.
 Wall C: 20.0 ft.
 Wall D: 24.0 ft.

	Sheathing*	Nail Size	Edge Nailing	Boundary Nailing		V_{allow}	HF/SPF Factor
Roof	7/16" OSB	8d	6 in. o.c.	12 in. o.c.	v = 180.0 plf	165.6 plf	0.92
Wall	3/8" Smartside	8d	6 in. o.c.	12 in. o.c.	v = 200.0 plf	164.0 plf	0.82
Wall	3/8" Smartside	8d	4 in. o.c.	12 in. o.c.	v = 300.0 plf	246.0 plf	0.82
Wall	3/8" Smartside	8d	3 in. o.c.	12 in. o.c.	v = 390.0 plf	319.8 plf	0.82

*Must be Rated sheathing

	V_{allow}	C_0	$2b_y/h$	edge nailing
Wall A: 311.6 plf	319.8 plf	C_0 = 1.00	1.00	3" o.c.
Wall B: 150.8 plf	164.0 plf	C_0 = 1.00	1.00	6" o.c.
Wall C: 187.0 plf	246.0 plf	C_0 = 1.00	1.00	4" o.c.
Wall D: 106.8 plf	164.0 plf	C_0 = 1.00	1.00	6" o.c.
Roof= 106.8 plf	165.6 plf			

Overturning Calculations

Wall A

Min. No. anchor bolts= 0
Width= 12.0 ft.
Height= 8.09 ft.
 $P_{wind} = 6,232 \text{ lbs.}$

Wall Weight= 594.48 lbs.

$Uplift_{wind} = 2,223.53 \text{ lbs.}$ Provide MR-88 Earth Anchor

Allowable Service, wind: N/A

Wall C

Min. No. anchor bolts= 0
Width= 20.0 ft.
Height= 8.09 ft.
 $P_{wind} = 6,232 \text{ lbs.}$

Wall Weight= 982.80 lbs.

$Uplift_{wind} = 1,021.06 \text{ lbs.}$ Provide MR-88 Earth Anchor

Allowable Service, wind: N/A

Wall B

Min. No. anchor bolts= 0
Width= 17.0 ft.
Height= 8.09 ft.
 $P_{wind} = 4,273 \text{ lbs.}$

Wall Weight= 957.18 lbs.

$Uplift_{wind} = 741.49 \text{ lbs.}$

Allowable Service, wind: N/A

Wall D

Min. No. anchor bolts= 0
Width= 24.0 ft.
Height= 8.09 ft.
 $P_{wind} = 4,273 \text{ lbs.}$

Wall Weight= 1,296.96 lbs.

$Uplift_{wind} = 215.74 \text{ lbs.}$

Allowable Service, wind: N/A

Building Uplift

Wind uplift= -31,250.84 lbs.
Min. building weight= 8,183.76 lbs.
Additional min. dead load= 0 lbs. additional dead load due to steel floor, wood base, or other permanent loads, if any, (not including foundation)
Net uplift= -23,067.08 lbs.
Total no. of anchor bolts (min.)= 0 (Does not include additional holdowns for overturning of the walls.)
Anchor bolt uplift= 0 lbs.

Additional anchors required Provide 9-MR-88 Earth Anchors

Bearing Wall Calculations

Axial Load

Stud Spacing= 16 in. o.c.
Max. Load on wall= 520.9 plf

depth= 3.50 in.
width= 1.50 in.

No. of members= 1

Length (depth)= 92.58 in.

Length (width)= 12.0 in.

$K_{e(x)} = 1$

$K_{e(y)} = 1$

$K_{cE} = 0.3$

$c = 0.8$

Load= 695 lbs.

Load per stud

$A = 5.25 \text{ sq.in.}$

$(l/d)_x = 26.45$

$(l/d)_y = 8.00$

$E'_{min} = 510,000 \text{ psi}$

Weak Axis Calculations(y)

$F_{cE} = 6550.31$

$F^*_c = 1653.13$

$F_{cE}/F^*_c = 3.96$

$1+F_{cE}/F^*_c/2c = 3.10$

$C_P = 0.94$

$F'_c = 1556.15$

$P_{allowable} = 8,170 \text{ lbs.}$

Good/No Good? **O.K.**

Lumber

SPF #1/#2

$F_b = 875 \text{ psi}$

$F_t = 450 \text{ psi}$

$F_v = 135 \text{ psi}$

$F_{cP} = 425 \text{ psi}$

$F_c = 1150 \text{ psi}$

$E_{min} = 510,000 \text{ psi}$

$E = 1,400,000 \text{ psi}$

Lumber Factors

$C_D = 1.25$

Duration for gravity load

$C_M = 1.00$

Wet Service

$C_t = 1.00$

Temperature

$C_L = 1.00$

Beam Stability

$C_F = 1.15$

Size for F_c

$C_{fu} = 1.00$

Flat Use

$C_i = 1.00$

Incising

$C_r = 1.15$

Repetitive Member

$C_r = 1.00$

Form

$C_T = 1.00$

Buckling Stiffness (NDS 4.4.2)

$C_F = 1.50$

Size for F_b

$C_D = 1.60$

Duration for lateral load

$C_r = 1.50$

Repetitive Member (wind)

Strong Axis Calculations (x)

$F_{cE} = 599.16$

$F^*_c = 1653.13$

$F_{cE}/F^*_c = 0.36$

$1+F_{cE}/F^*_c/2c = 0.85$

$C_P = 0.33$

$F'_c = 545.44$

$P_{allowable} = 2,864 \text{ lbs.}$

Good/No Good? **O.K.**

Wind Load

Wind load per stud= 60.6 plf
Moment= 5,412 in.-lbs.
Reaction= 234 lbs.

Header depth= 3.50 in.

Total header width= 1.50 in.

Header span= 8.0 ft.

Bending

$S_x = 3.06 \text{ cu.in.}$

$F_b = 3150 \text{ psi}$

$f_b = 1767 \text{ psi}$

Good/No Good? **O.K.**

Shear

$F_v = 216 \text{ psi}$

$f_v = 67 \text{ psi}$

Good/No Good? **O.K.**

Combined Bending and Axial Loading

$F'_c = 698.17$

combine allowable compressive stress

$f_c = 66 \text{ psi}$

combine compressive stress

Combined stress index= 0.64

Good/No Good? **O.K.**